

Verification of the Thermal Performance of the HEMJ Divertor

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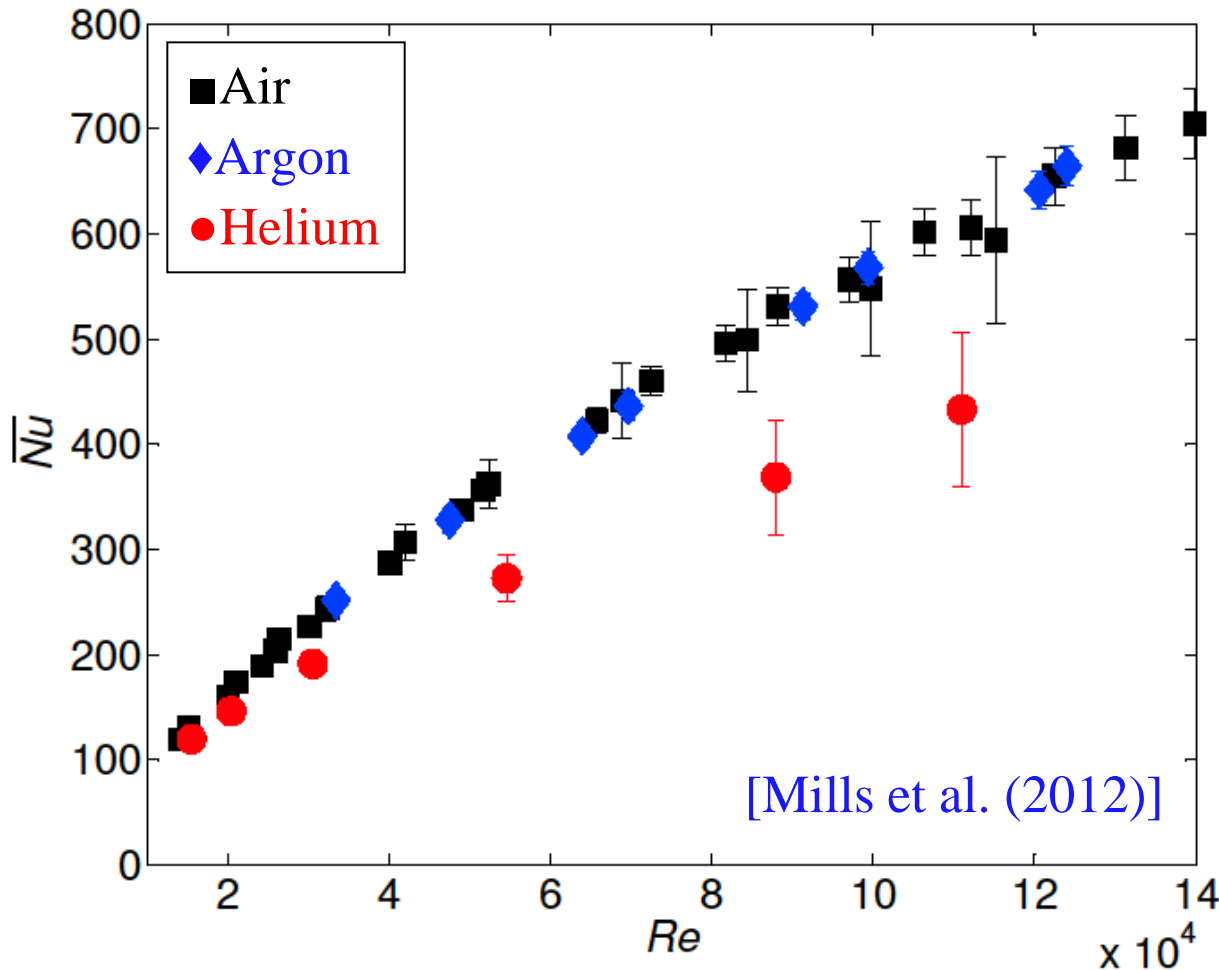
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Objectives

- Update previous predictions of the thermal performance of the helium-cooled multi-jet (HEMJ) modular divertor design
 - Recent results on finger-type divertor \Rightarrow dynamic similarity requires matching non-dimensional coolant flow rate Re and ratio of divertor to coolant thermal conductivities
- Perform experiments on steel and brass HEMJ-like test sections cooled by helium, air, or argon
 - Incident heat fluxes $q'' \leq 3 \text{ MW/m}^2$
- Following previous approach, extrapolate results to prototypical conditions to obtain parametric design curves for HEMJ
 - Max. heat flux q''_{max} at given max. pressure boundary temperature
 - Pressure drop (loss coefficient K_L) at prototypical Re

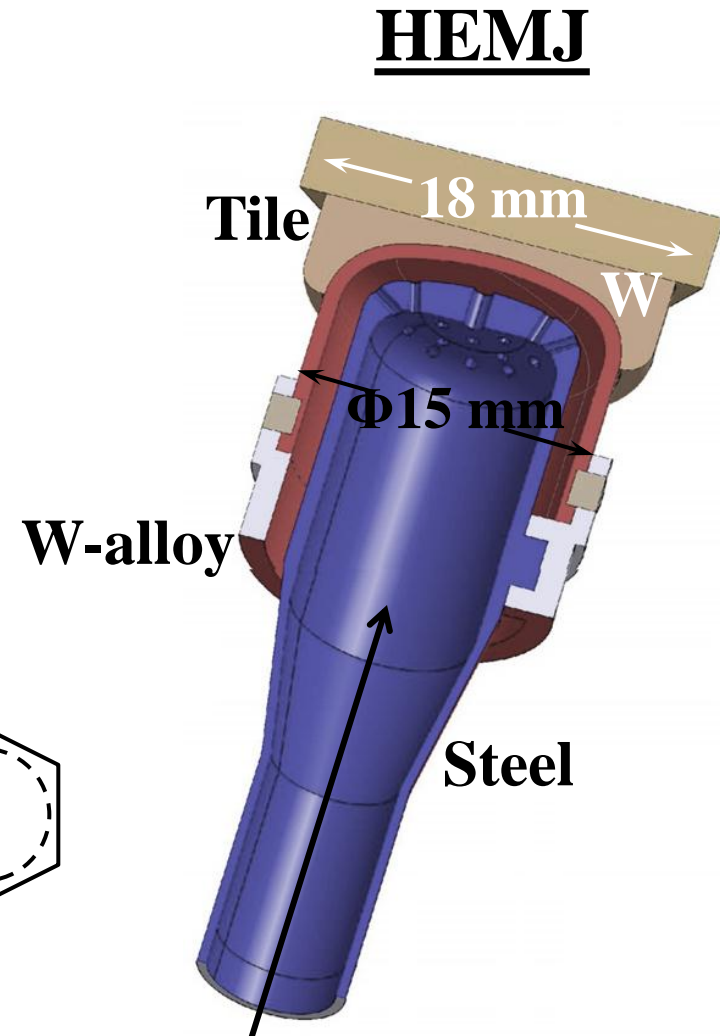
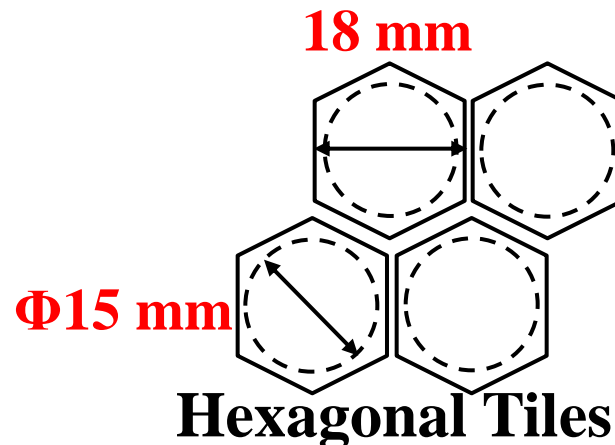
Previous Experiments



- Experiments with He and Ar to validate procedure
- He Nu did not match air, Ar Nu
- Similarity not achieved matching only Re
- Account for changes in conduction vs. convection
- Thermal conductivity ratio, κ

HEMJ Divertor

- Accommodate $q'' > 10 \text{ MW/m}^2$
[Ihli et al. 05; Weathers 07; Crosatti 08]
 - Hot He enters at 10 MPa, cools W tile as an array of impinging jets
 - Require many modules ($\sim 5 \times 10^5$ for HEMJ) to cover $O(100 \text{ m}^2)$ divertor

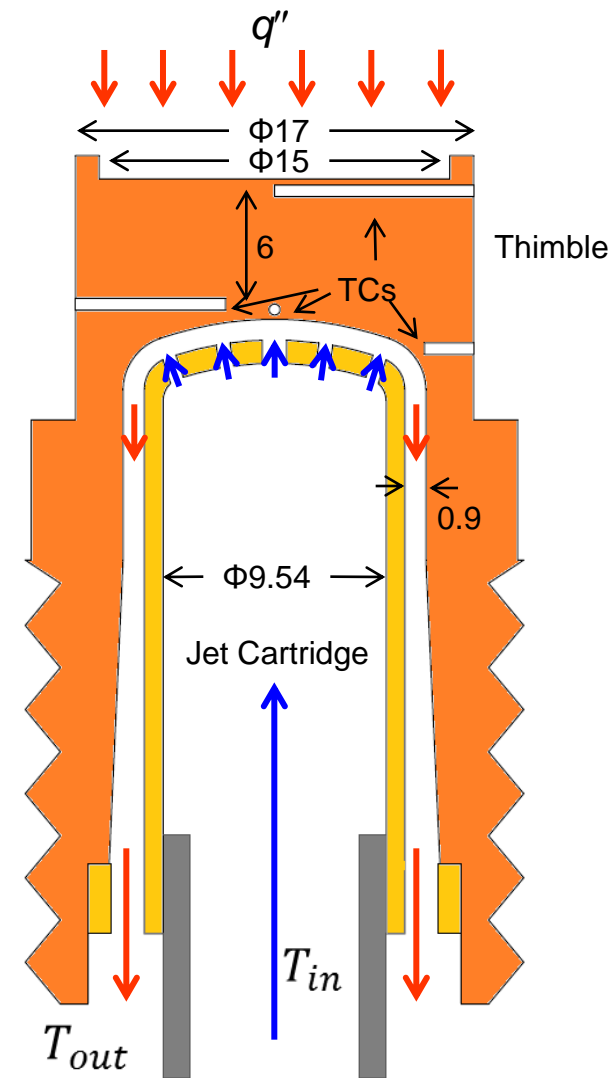


GT Test Module

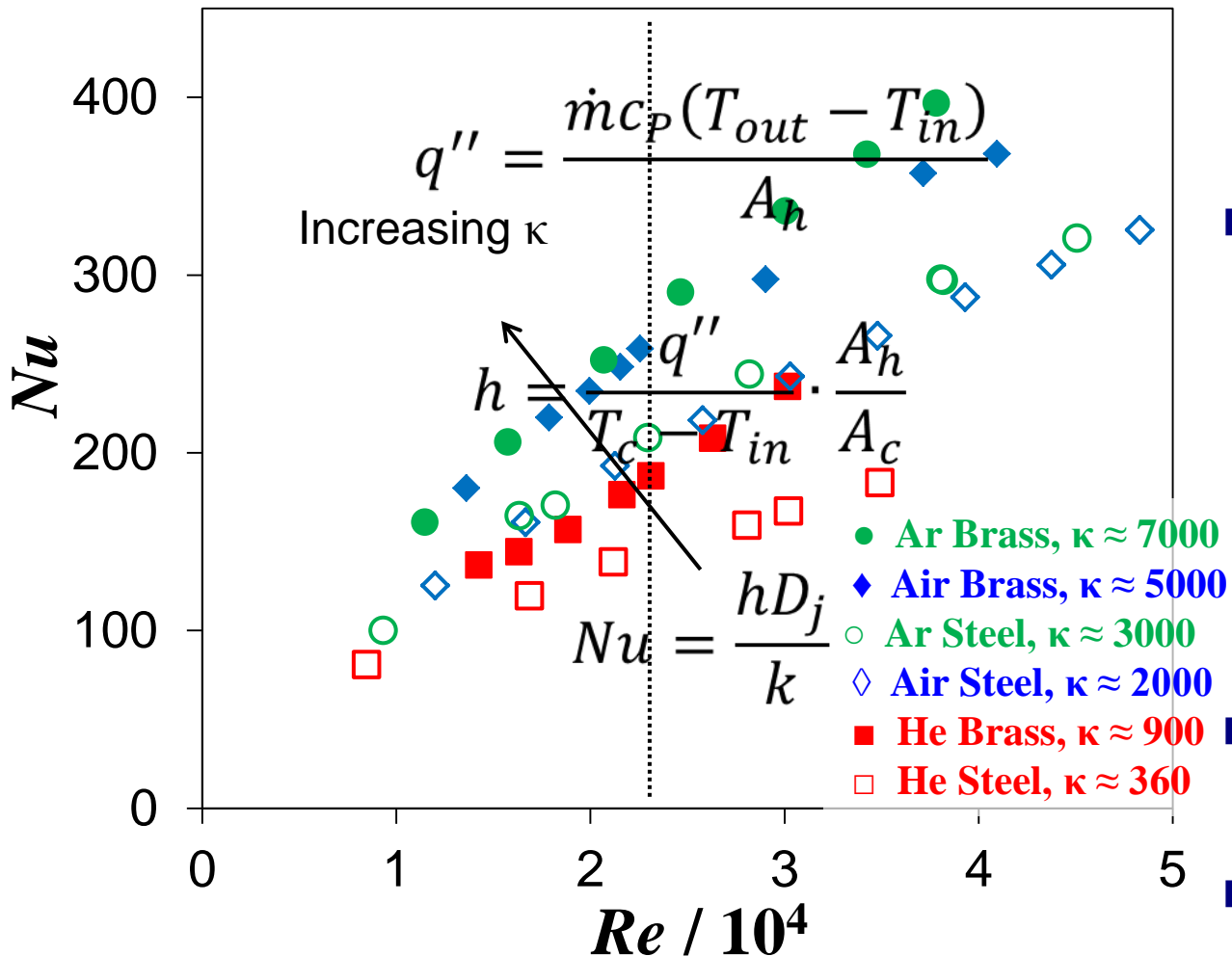
- Brass and steel thimbles (pressure boundary) cooled by helium (He), air, argon (Ar) at near-ambient temperatures

- Prototypical conditions: $Re = 2.16 \times 10^4$ (mass flow rate $\dot{m} = 6.8$ g/s), $\kappa = 340$
- Experiments: $Re = 8 \times 10^3 - 6 \times 10^4$
 $\kappa \equiv k_s / k = 360 - 7000$
- Incident heat flux $q'' \leq 3.0$ MW/m² (torch), $q'' \leq 0.9$ MW/m² (electrical)
- Measure temperatures near cooled surface with embedded thermocouples (TC) $\Rightarrow T_C$, pressure drop across module Δp

$$Re = \frac{\dot{m} D_j}{A_j \mu_i}$$

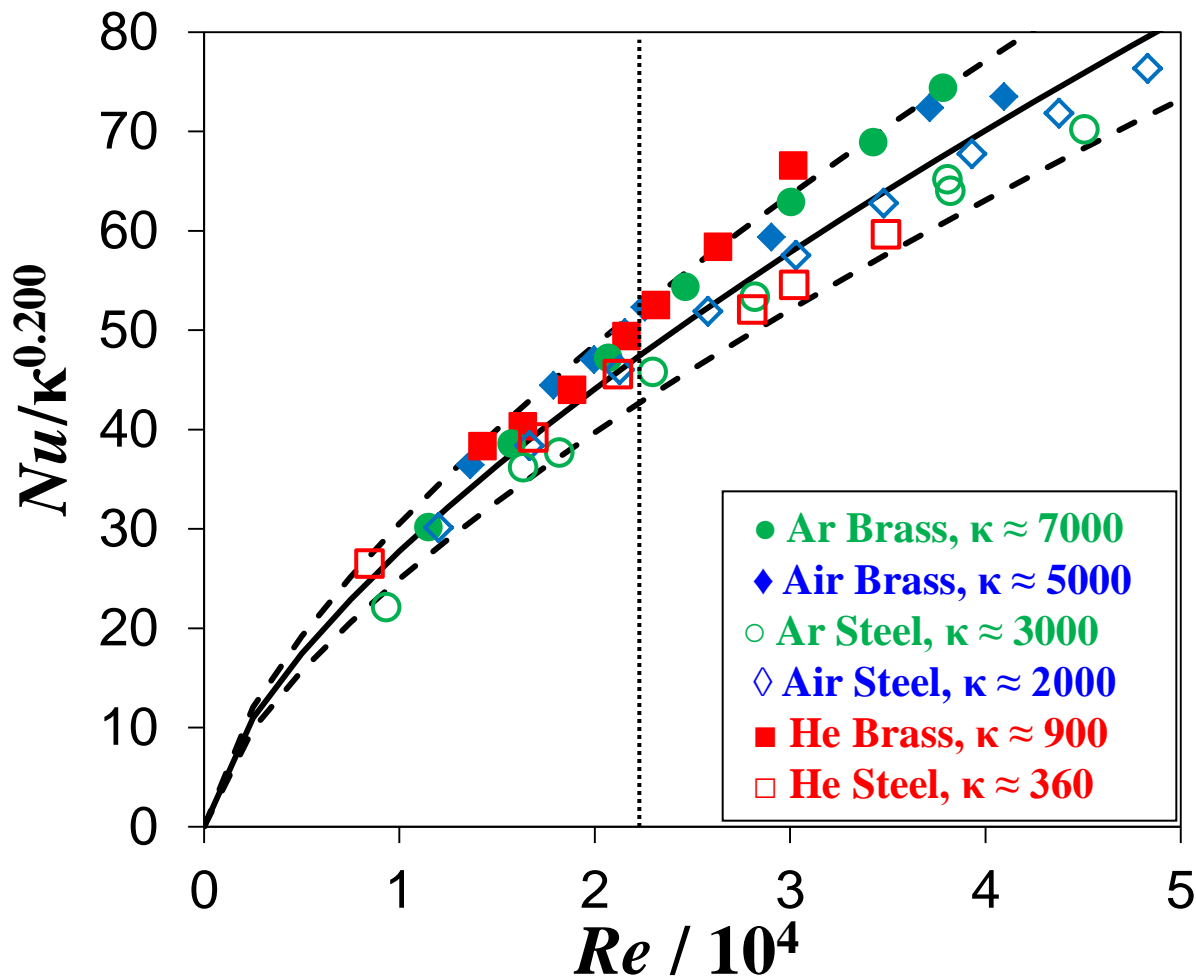


Nu v Re



- Heat flux based on energy balance of coolant
- HTC assumes all heat absorbed through cooled surface
 - Doesn't take conduction into account
- Each scenario shows its own trend
- Cases arranged by κ

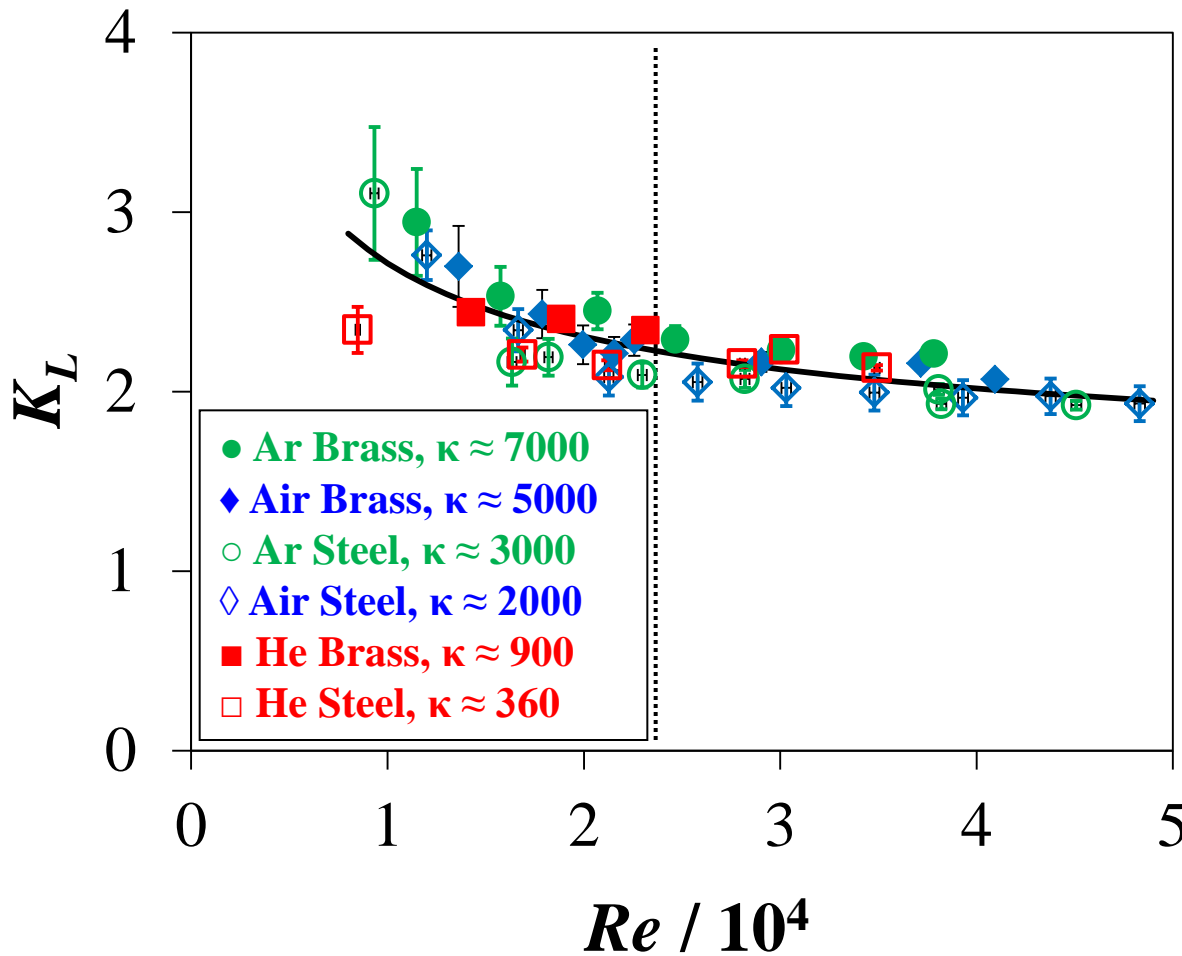
Accounting for κ



- Multilinear curve fitting assuming power law
- Nearly all data fits within $\pm 10\%$
- Prototypical values:
 - $Re = 21,600$
 - $\kappa = 340$

$$Nu = 0.056 \cdot Re^{0.666} \kappa^{0.200}$$
$$R^2 = 0.96$$

Pressure Loss Coefficient



- Pressure loss coefficient K_L

$$K_L = \frac{\Delta p}{\frac{1}{2}\rho V^2}$$

- Hydraulic parameter independent of κ
- Correlate to Re

$$K_L = 1.39 \cdot \left(Re / 10^4 \right)^{-0.50} + 1.32$$

Prototypical Conditions

- Use $Nu = f(Re, \kappa)$ and $K_L = f(Re)$ to calculate performance for a range of high pressure/temperature operating conditions

- Lines of constant pressure boundary temperature, T_s ,

- Use Nu correlation to calculate q''_{\max}

- $T_{\text{in}} = 600 \text{ }^\circ\text{C}$

- $T_s = 1200 \text{ }^\circ\text{C}$

$$q''_{\max} = \frac{T_s - T_{\text{in}}}{R_T} \quad 1.25 q''_t = q''$$

- Area changes result in q'' focusing from tile to pressure boundary

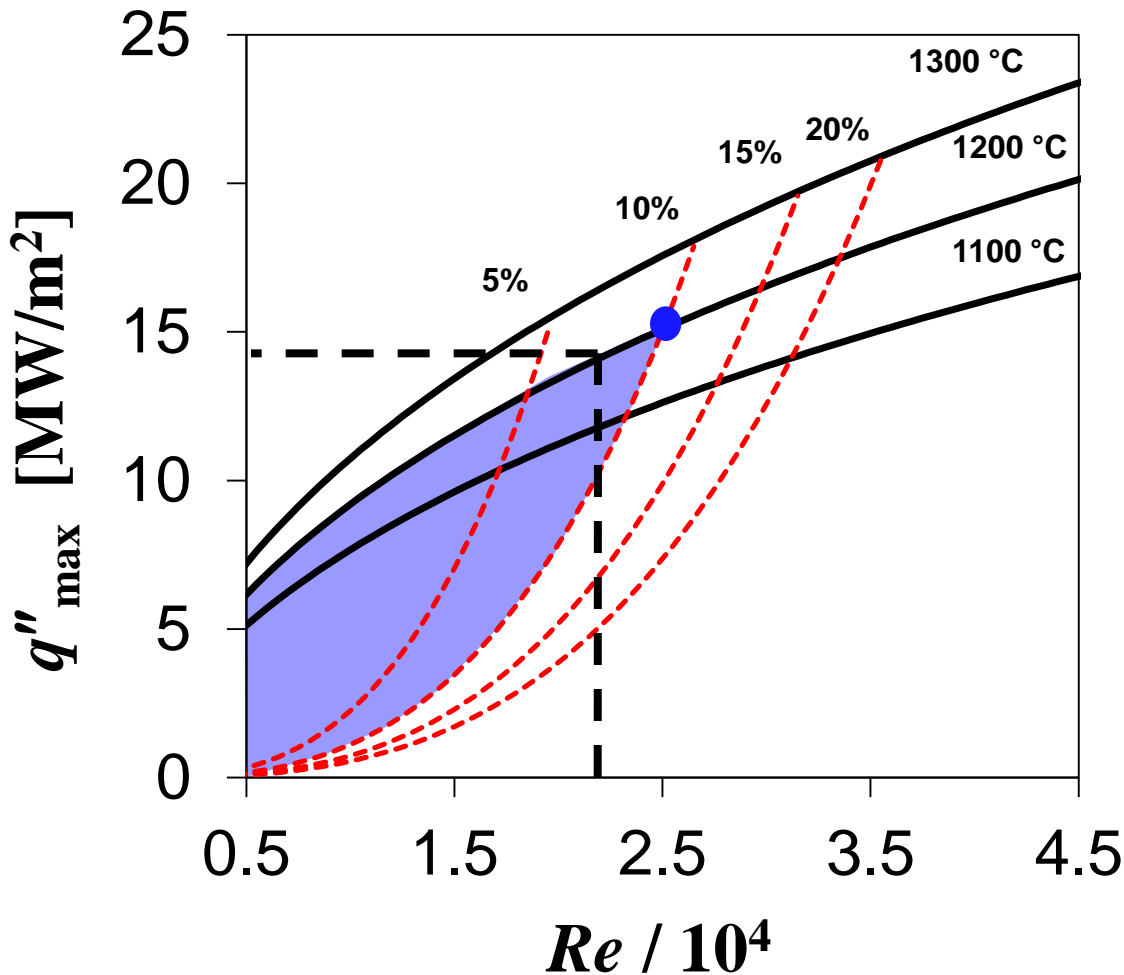
- Loss coefficient K_L gives pressure drop for prototype Δp_p

- Lines of constant pumping power as fraction of incident thermal power, β

- Desire to have $\beta < 10\%$

$$\beta = \frac{\dot{m} \Delta p_p}{\bar{\rho} q'' A_h}$$

Performance Curves



- For $\dot{m}_{He} = 6.8$ g/s
 $Re = 2.16 \times 10^4$
 - $\beta \approx 8\%$
 - $q'' \approx 14.1$ MW/m²
 - $q''_t \approx 11.4$ MW/m²
- For $\beta < 10\%$ and
 $T_s < 1200$ °C
 - $Re < 2.5 \times 10^4$
 - $q'' < 15.5$ MW/m²
 - $q''_t < 13$ MW/m²

Summary

- Seven experimental configurations
 - HEMJ shows similar conduction/convection characteristics as the previous finger-type design
- Parametric design curves were created to aid in further design iterations and to account for changes in operating conditions
 - For $\beta < 10\%$ and $T_s < 1200\text{ }^\circ\text{C} \rightarrow Re < 2.5 \times 10^4$, $q'' < 15.5\text{ MW/m}^2$ and $q_t'' < 13\text{ MW/m}^2$
- These studies show that thermal conductivity ratio methodology can be applied to other divertor designs with similar geometries/heat transfer paths
 - Performance verification with dynamically similar experiments over a wide range of conditions